

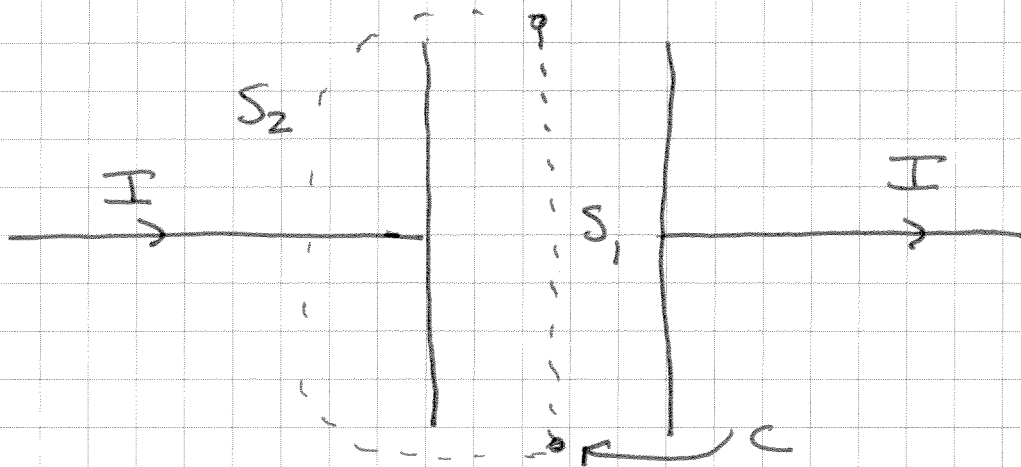
# Ampere's Law for Electrodynamics

Ampere's Law

$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 I_{enc}$$

is incomplete.

Consider charging a capacitor with current  $I$   
and two ~~cores~~  $C_1$  and  $C_2$ .



Surfaces  $S_1$  and  $S_2$  bounded by the same curve  $C$ .

The current enclosed for  $S_1$ ,  $I_{enc,1} = 0$

but the current enclosed for  $S_2$ ,  $I_{enc,2} = I$ .

This means  $\oint \vec{B} \cdot d\vec{l}$  has two different values which is not allowed.

In an analogy to Faraday's Law, one might consider fixing this inconsistency with the time rate of change of electric flux.

The electric flux through surface  $S_1$  is

$$\Phi_e = EA$$

where  $A$  is the area of the plate and  $E$  the electric field.

$$\frac{d\Phi_e}{dt} = A \frac{dE}{dt} \qquad E = \frac{\sigma}{\epsilon_0}$$

$$= \frac{d}{dt} A\sigma/\epsilon_0$$

$$= \frac{1}{\epsilon_0} \frac{dQ}{dt} = \frac{I}{\epsilon_0}$$

So  $\epsilon_0 \frac{d\Phi_e}{dt}$  is zero on surface 2 and

$I$  on surface 1, just what we need.

Defn Displacement Current ( $I_d$ ) A quantity with dimensions of current needed to complete Ampere's Law.

$$I_d = \epsilon_0 \frac{d\Phi_e}{dt}$$

Ampere's Law (Complete)

$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 (I_{enc} + I_d)$$

$$= \mu_0 \int_S \vec{J} \cdot d\vec{\sigma} + \mu_0 \epsilon_0 \frac{d}{dt} \int_S \vec{E} \cdot d\vec{\sigma}$$

Differential Form

$$\nabla \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

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An alternate method of identifying the need to fix Ampere's Law.

## Ampere's Law

$$\nabla \times \vec{B} = \mu_0 \vec{J}$$

Take the divergence; the divergence of a curl is always zero

$$\nabla \cdot (\nabla \times \vec{B}) = \mu_0 \nabla \cdot \vec{J} = 0$$

For magnetostatics,  $\nabla \cdot \vec{J} = 0$  and everything is good, but in general

$$\nabla \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0 \quad (\text{continuity eqn})$$

$$\Rightarrow \nabla \cdot \vec{J} \neq 0$$

$$\text{but } \nabla \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0.$$

So maybe

$$\nabla \cdot \nabla \times \vec{B} = \mu_0 \left( \nabla \cdot \vec{J} + \frac{\partial \rho}{\partial t} \right)$$

Use Gauss' Law

$$\nabla \cdot \vec{E} = \rho / \epsilon_0 \quad \Rightarrow \quad \rho = \epsilon_0 \nabla \cdot \vec{E}$$

$$\nabla \cdot (\nabla \times \vec{B}) = \mu_0 \left( \nabla \cdot \vec{J} + \epsilon_0 \nabla \cdot \frac{\partial \vec{E}}{\partial t} \right)$$

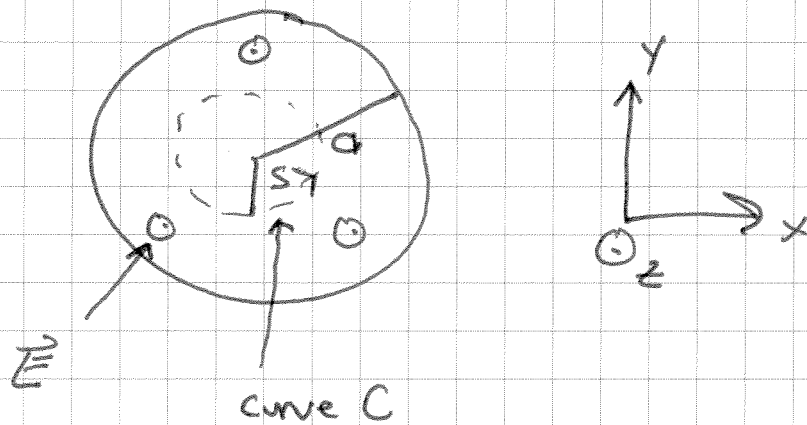
so Ampere's Law is fine if

$$\nabla \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

$\Rightarrow$  The displacement current acts as a source in Ampere's Law just like a real current.

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Ex A cylindrical  $s < a$  contains a time varying electric field  $\vec{E} = E_0 e^{-t/\tau} \hat{z}$



The electric flux through a circular surface of radius  $s < a$  is

$$\begin{aligned} \Phi_e &= EA = E\pi s^2 \\ &= E_0 \pi s^2 e^{-t/\tau} \end{aligned}$$

$\Rightarrow$  Note, convention for positive normal used

## Displacement Current

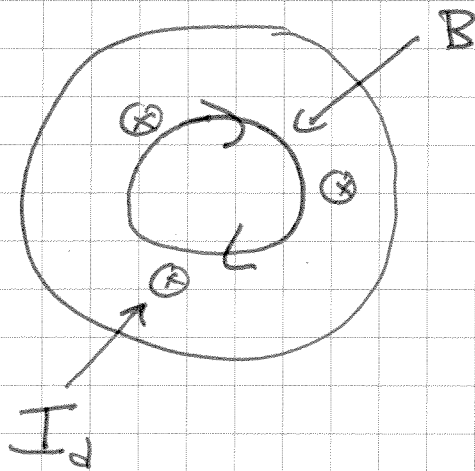
$$\underline{I}_d = \epsilon_0 \frac{d\Phi_e}{dt}$$

$$= - \frac{\epsilon_0 \pi s^2}{\tau} e^{-t/\tau}$$

$\Rightarrow$  - sign indicates  $\underline{I}_d$  directed into the page.

Since  $\underline{I}_d$  is cylindrically symmetric, the magnetic field generated by  $\underline{I}_d$  is circular about the axis.

The Right Hand rule still gives the direction



Ampere  $\oint \vec{B} \cdot d\vec{l} = \mu_0 (I_{enc} + I_d) = \mu_0 I_d$

$$= 2\pi s B$$

$$B = \frac{\mu_0 I_d}{2\pi s} = \frac{\mu_0}{2\pi s} \left( -\frac{\epsilon_0 E_0 \pi s^2}{\tau} e^{-t/\tau} \right)$$

$$\vec{B} = \frac{-\epsilon_0 \mu_0 E_0 s}{2\tau} e^{-t/\tau} \hat{\phi} \quad s < a$$

Outside Region  $s > a$

$$\Phi_e = \pi a^2 E$$

$$I_d = \epsilon_0 \frac{d\Phi_e}{dt} = -\frac{\pi a^2 E_0}{\tau} e^{-t/\tau}$$

$$\vec{B} = \frac{\mu_0 I_d}{2\pi s} \hat{\phi} = -\frac{a^2 E_0}{2s\tau} e^{-t/\tau} \hat{\phi}$$


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We can also define a displacement current density

$$\vec{J}_d = \epsilon_0 \frac{d\vec{E}}{dt}$$

For the above system

$$\vec{J}_d = -\frac{\epsilon_0}{\tau} E_0 e^{-t/\tau} \hat{z} \quad s < a$$

and then

$$I_d = \int_S \vec{J}_d \cdot d\vec{a} = J_d A$$

$$= \frac{-\epsilon_0 \pi s^2 E_0}{T} e^{-t/T}$$